



POLARIS
SEMICONDUCTOR

Efficient DC Voltage Conversion Without Switching

*A Path to Extremely Compact and Low
Noise DC Voltage Regulators*

Matthew Lumb, Founder



Polaris Background

- ◆ Founded late 2018 – based in Northern Virginia
- ◆ Fabless semiconductor startup
- ◆ Pre-revenue – funding via various non-dilutive grants
- ◆ **About me:** Spent 10 years in Optoelectronics and Radiation Effects Branch at NRL
- ◆ Optoelectronics and semiconductor device specialist





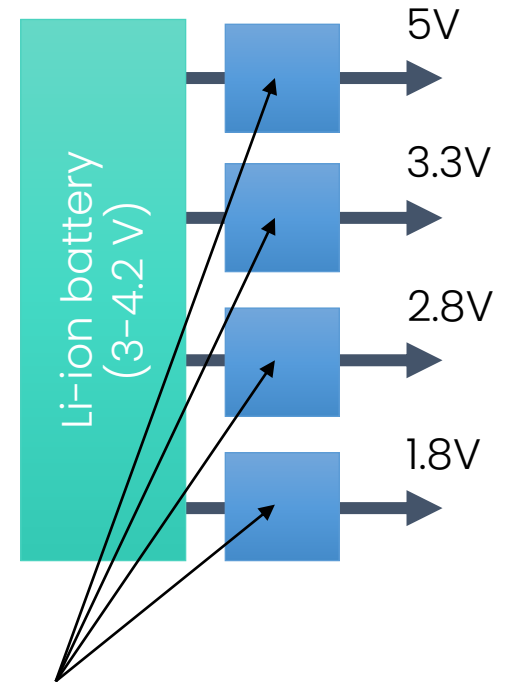
Introduction

DC Voltage Regulator

- ◆ Converts unregulated DC input to regulated DC output
- ◆ Powers a wide range of digital & analog loads

Requirements for Defense/Space:

- ◆ **Low noise** – minimize electromagnetic interference (EMI)
- ◆ **SWaP** – minimize footprint and mass
- ◆ **Efficient** – minimize heating and maximize battery life
- ◆ **Radiation hard** – able to endure harsh space radiation environment



Voltage regulators



Polaris Technology

Switching Regulator

Advantages

- ✓ Boost and buck voltage
- ✓ High efficiency

Pains

- ✗ Generates EMI
- ✗ Large footprint and component count

Linear Regulator

Advantages

- ✓ No EMI
- ✓ Very compact

Pains

- ✗ Buck voltage only
- ✗ Inefficient for large voltage steps

Polaris Semiconductor Technology

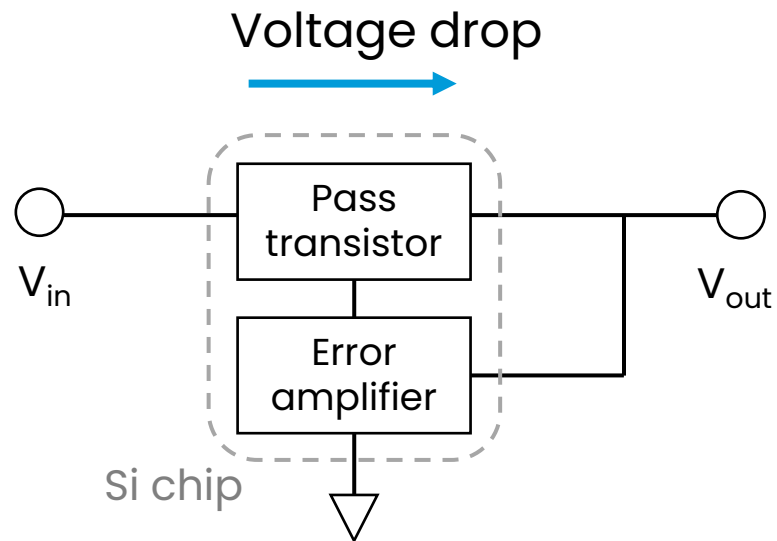
- ✓ Linear regulator with functionality of a switching regulator
- ✓ Boost & buck voltage, no EMI, very compact, high efficiency (65-85%)



How it Works

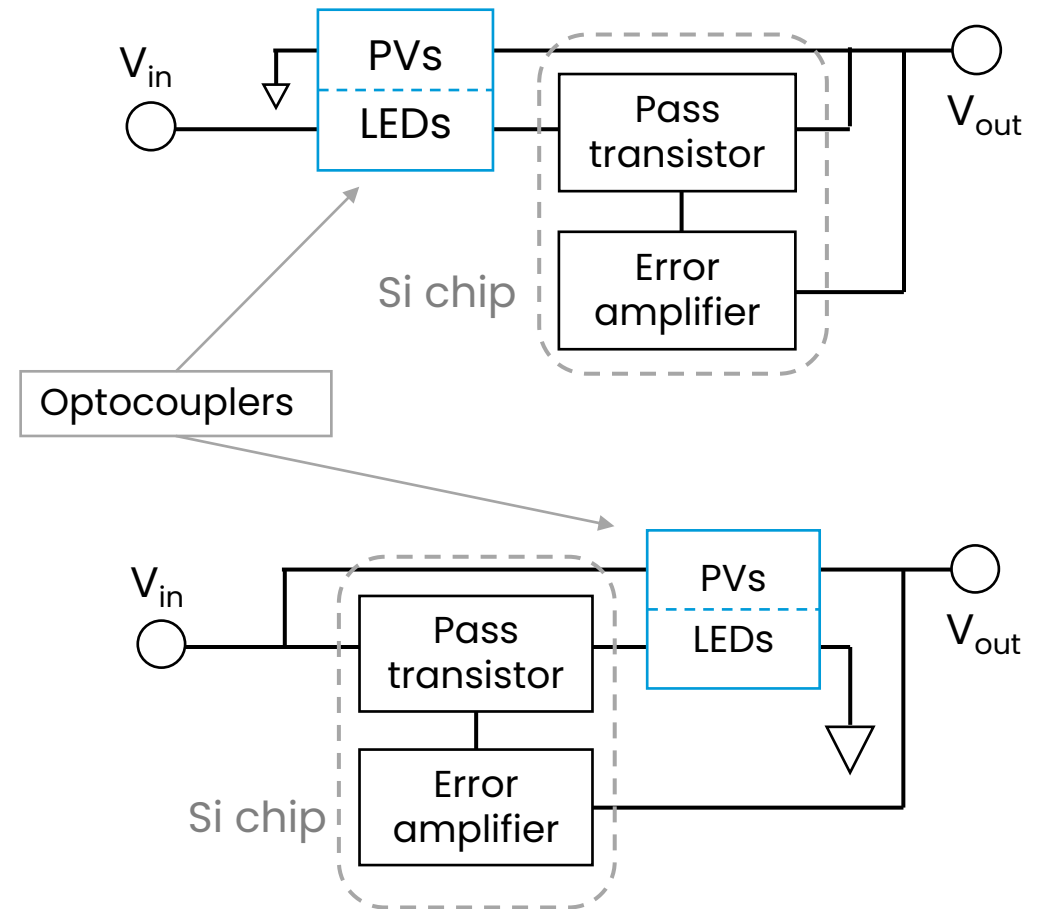
Standard Linear Regulator

- ◆ Controlled voltage drop across pass transistor



Polaris Semiconductor Regulator

- ◆ Uses photons to raise or lower voltage

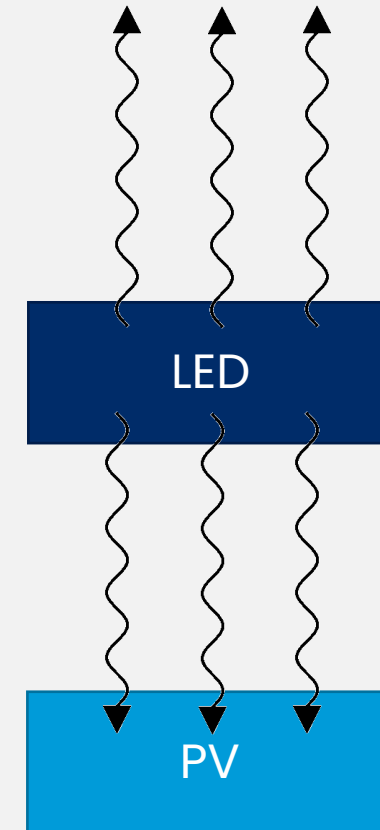




High Efficiency

- ◆ **A problem:** typical optocoupler is 1-2% efficient
- ◆ Three main losses:
 - ◆ Undirected emission
 - ◆ Reflection and escape cone losses
 - ◆ Spectral mismatch of LED and PV

PV Output Optocoupler Device

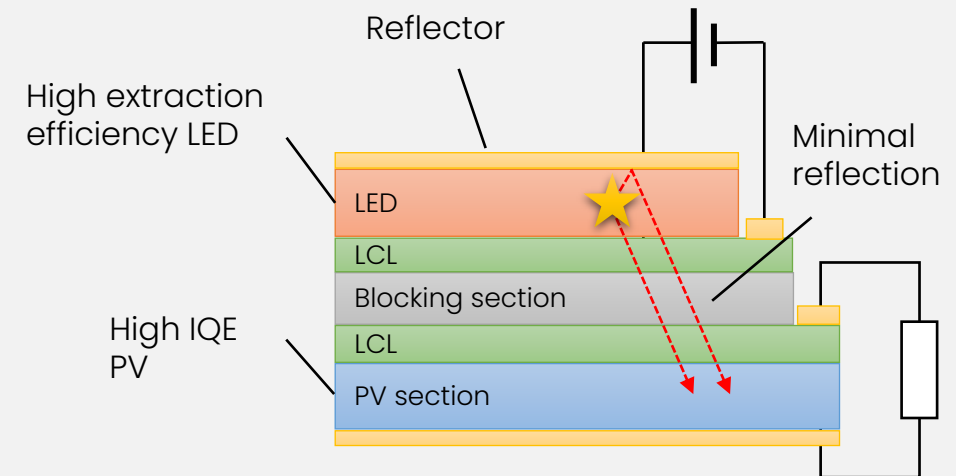




High Efficiency

- ◆ **A problem:** typical optocoupler is 1-2% efficient
- ◆ Three main losses:
 - ◆ Undirected emission
 - ◆ Reflection and escape cone losses
 - ◆ Spectral mismatch of LED and PV
- ◆ **Our solution:** novel GaAs-based monolithic optocoupler device
- ◆ Manufacture identical to GaAs LEDs, VCSELs etc.

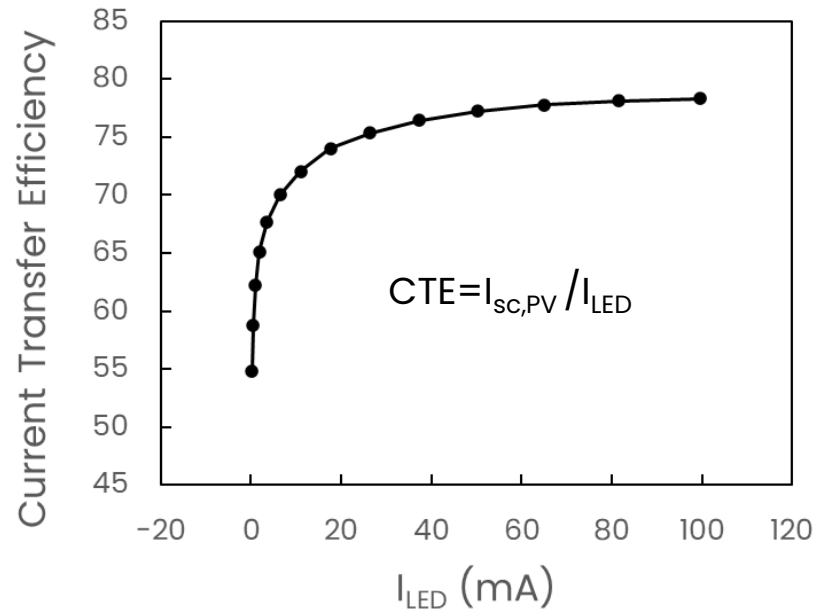
PV Output Optocoupler Device



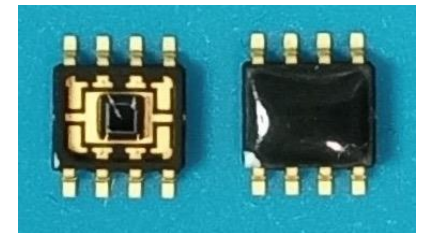
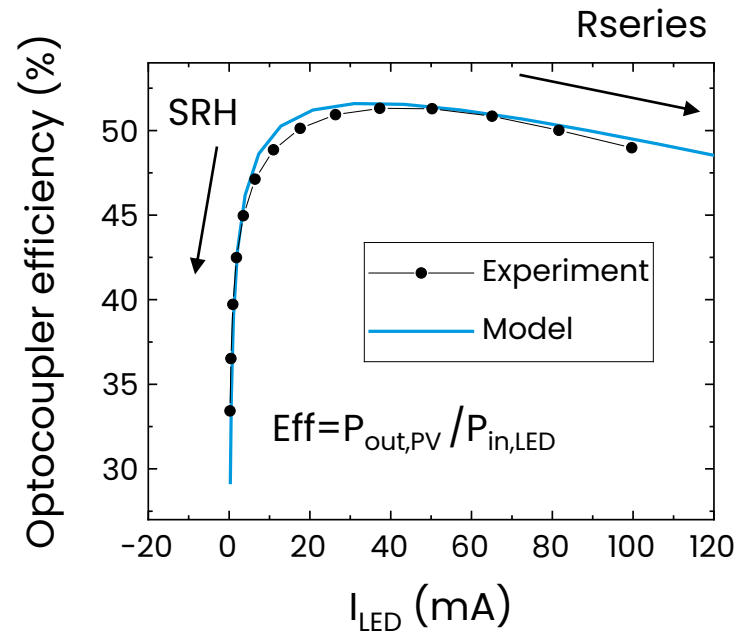
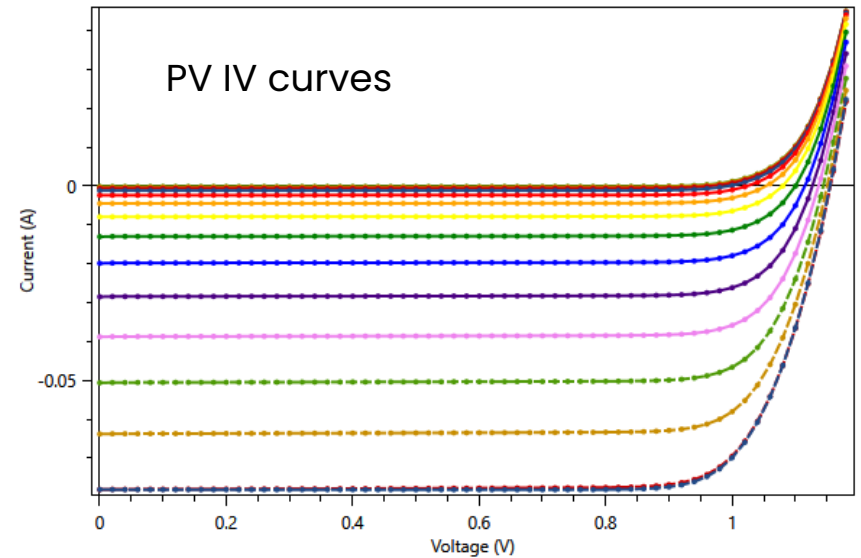


Optocoupler Performance

- ◆ Peak efficiency of optocoupler is 52%
- ◆ Close to 80% current transfer at high forward bias
- ◆ Future efficiency improvements, clear path to 60%



Increasing I_{LED}



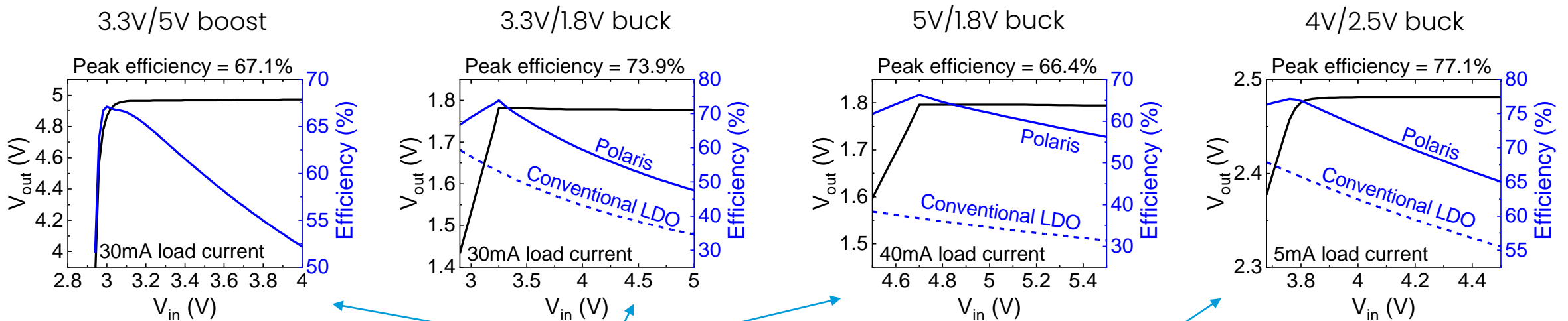
SOIC-8 packages
 52% optocoupler efficiency
 (NSF Phase I data)
 Path to >60%



Non-rad-hard prototypes

- ◆ Built a range of proof-of-concept chips, some packaged, some at breadboard level
- ◆ Possibility for bypass operation
- ◆ Can also achieve galvanic isolation

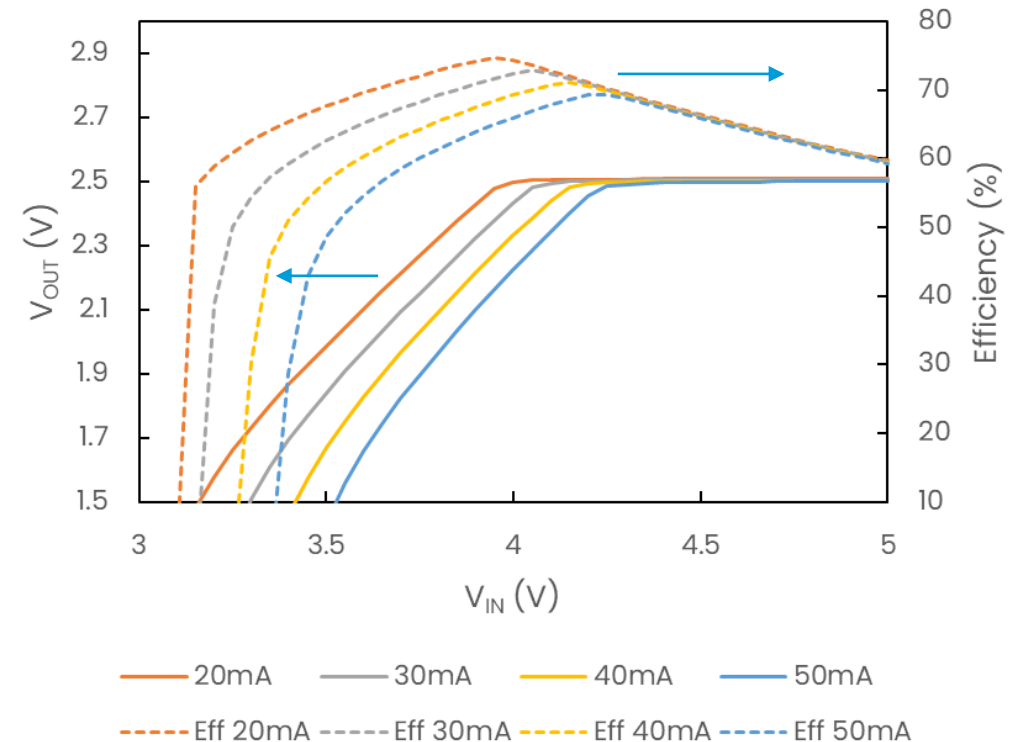
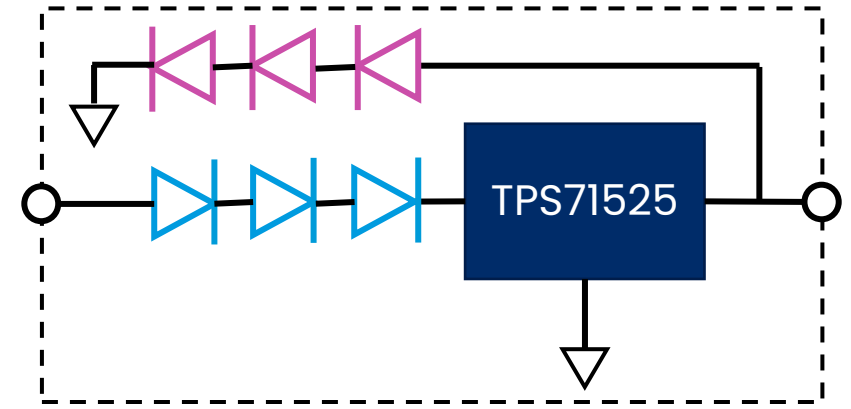
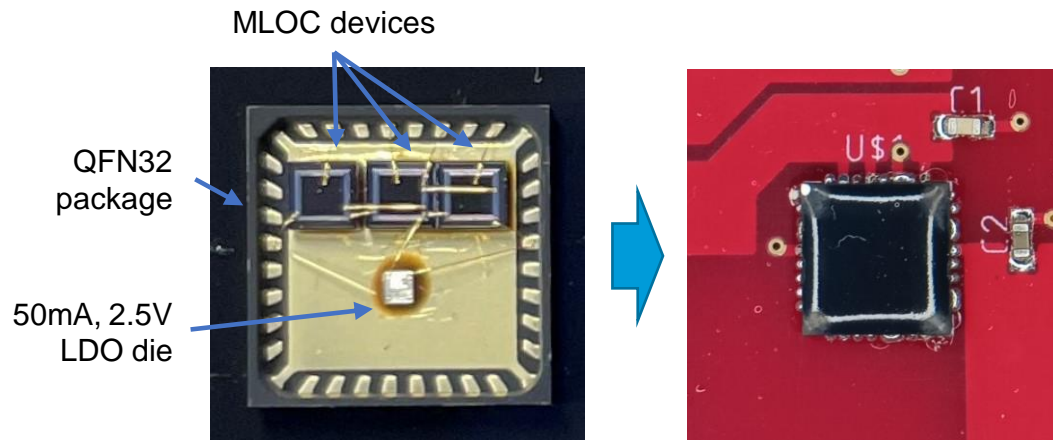
Voltage in / Voltage out	Polaris regulator efficiency	Linear regulator efficiency	Relative improvement
3.3V/5V (boost)	67%	N/A	N/A
4V/2.5V	77%	66%	17%
3.3V/1.8V	74%	53%	40%
5V/1.8V	66%	36%	80%





Performance - 2.5V buck

- ◆ Texas Instruments TPS71525 LDO co-packaged with optocouplers
- ◆ TPS71525: 50mA, 2.5V fixed output LDO
- ◆ Co-packaged with optocouplers in 7mm QFN32 plastic packages
- ◆ Not optimized for size!

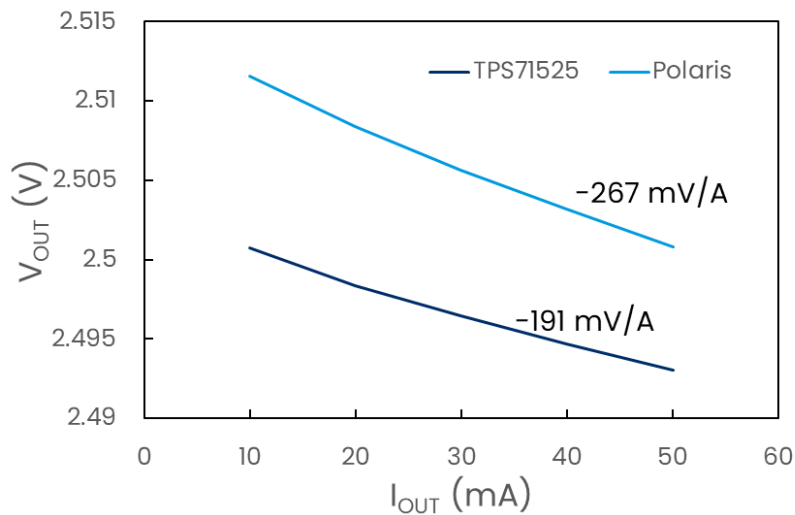




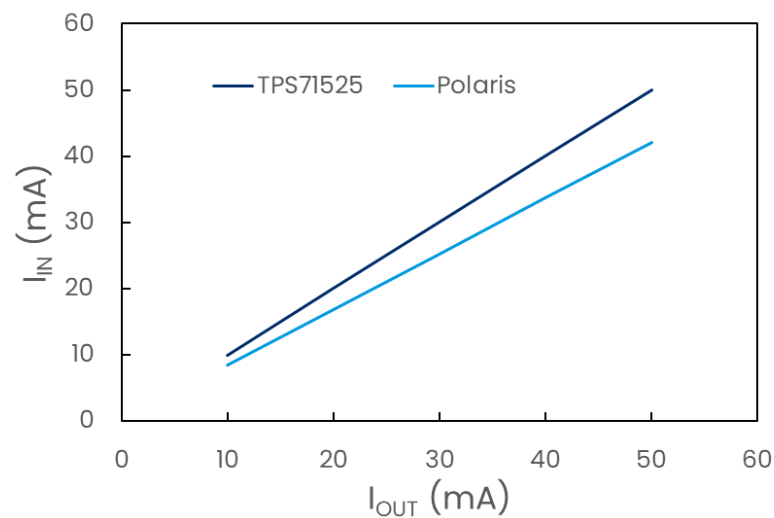
Comparison - 2.5V buck

- ◆ Comparison of standard TPS71525 to Polaris device at $V_{IN} = 5V$, $V_{OUT} = 2.5V$
- ◆ Comparable load regulation - within datasheet specs of 440 mV/A
- ◆ Lower input current for Polaris device - optocoupler effect
- ◆ ~20% rel. higher efficiency at $V_{IN} = 5V$ - efficiency advantage increases for larger V_{IN}/V_{OUT} ratios

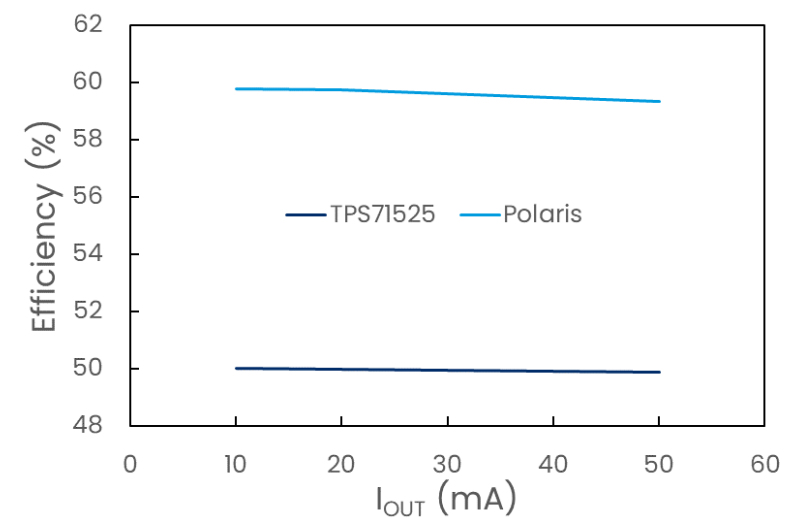
Load regulation $V_{IN} = 5V$



Input current $V_{IN} = 5V$



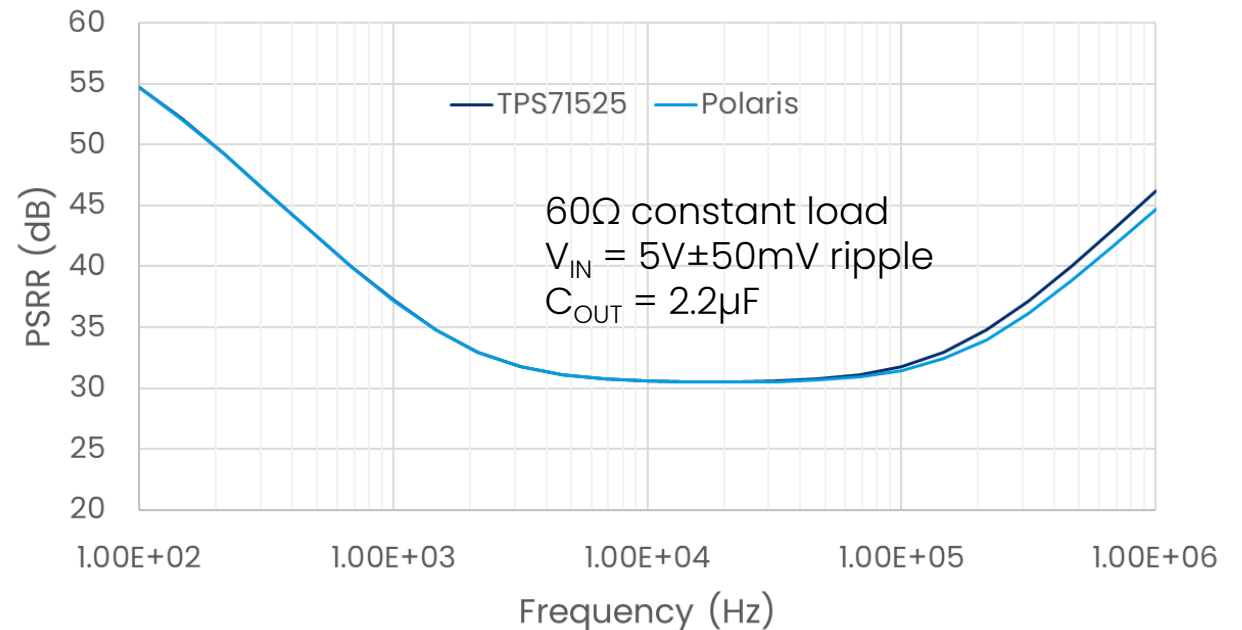
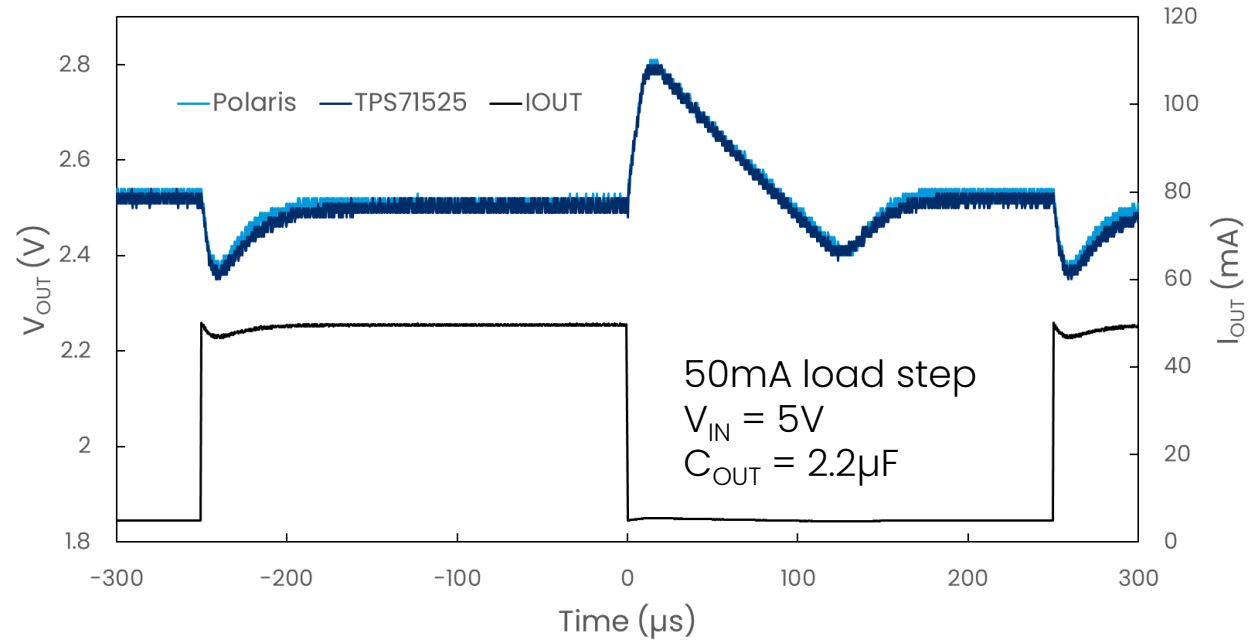
Efficiency $V_{IN} = 5V$





Transient Response - 2.5V buck

- ◆ Load step measurements of 2.5V buck regulator containing TPS71525
- ◆ Compared to TPS71525 LDO
- ◆ Virtually identical load step response!
- ◆ SPICE simulation of PSRR – slightly lower PSRR at high frequency with optocouplers
- ◆ Presently arranging testing of PSRR





Rad-hard Prototypes

- ◆ RF Micropower supplied LDOs, $I_{OUT} < 300\text{mA}$
- ◆ Two configurations – 5V/1.8V buck, 3.3V/5V boost
- ◆ No external caps required

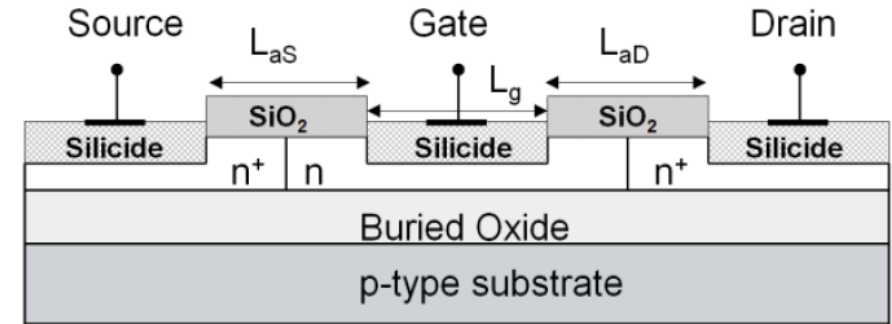
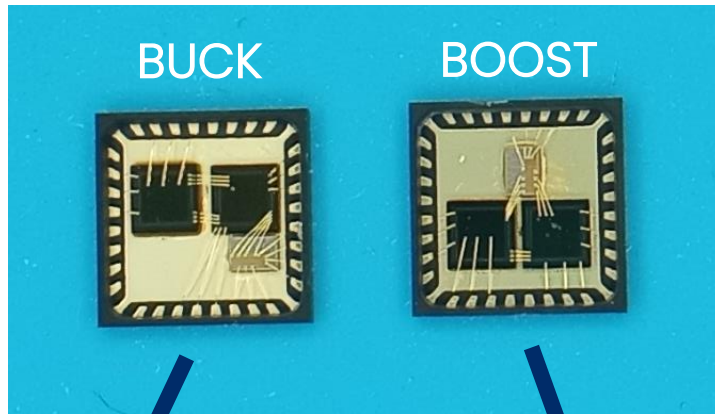


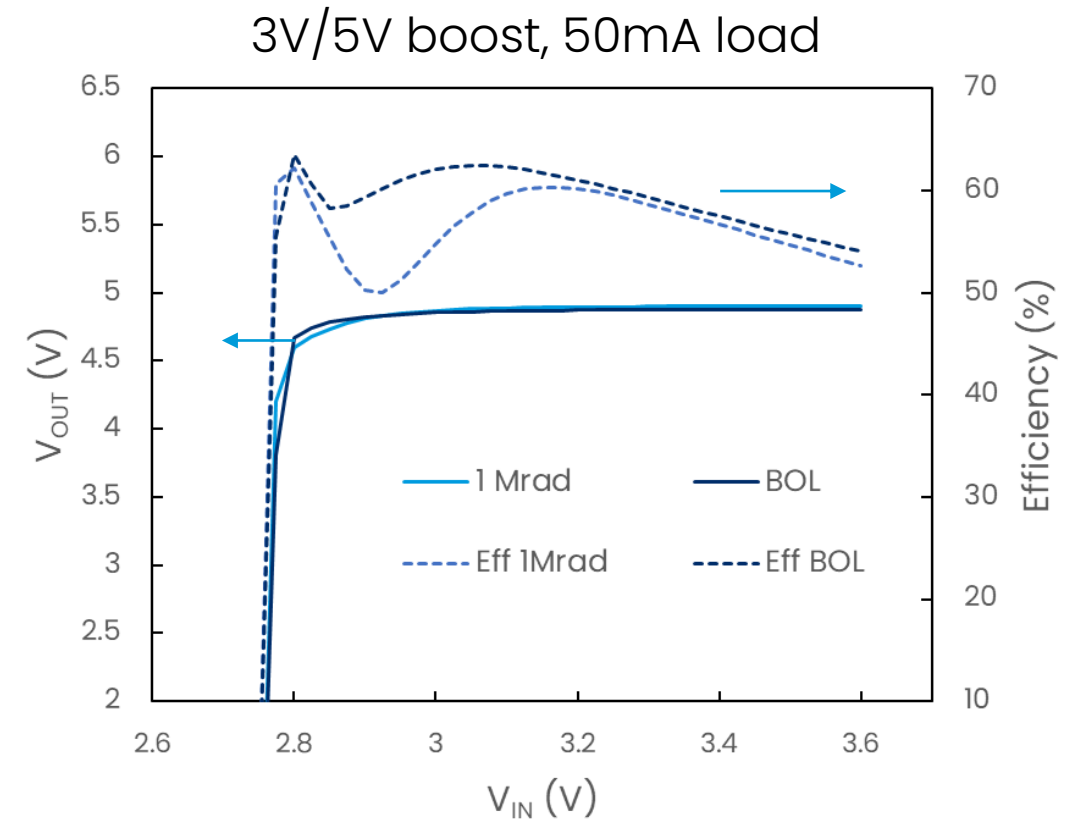
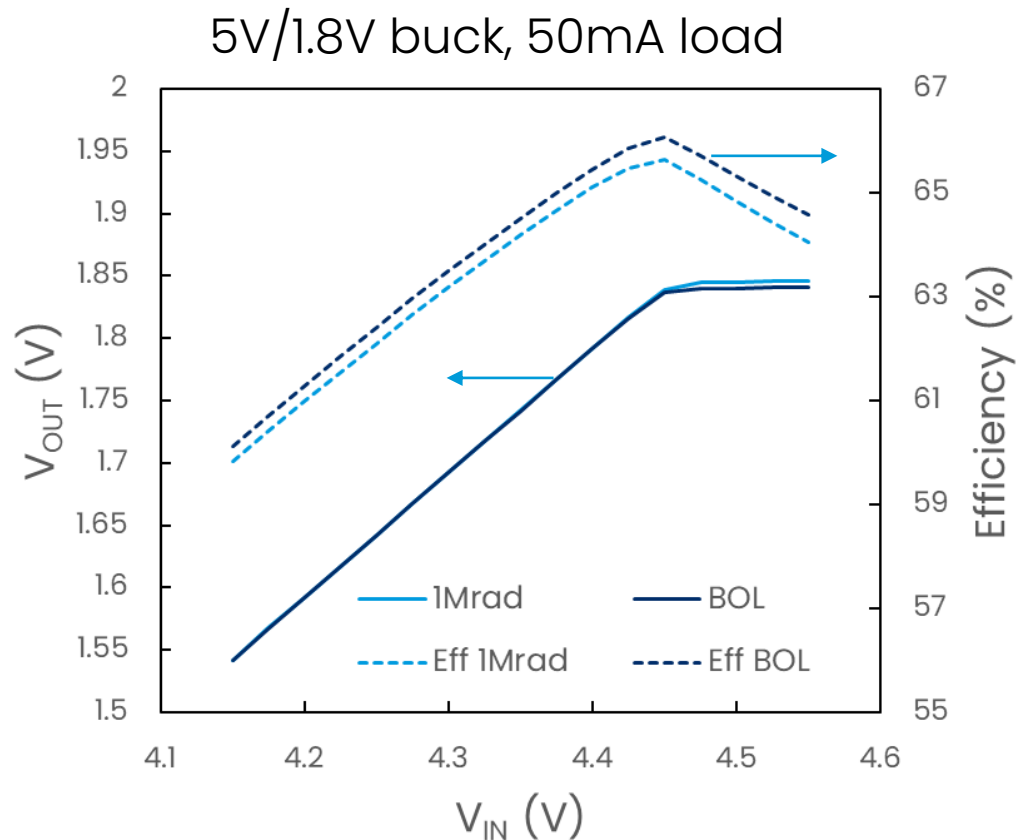
Fig. 1. Schematic cross-section of the SOI MESFET. The Schottky gate of the MESFET is formed using the silicide step that creates the low resistance source drain contacts. Spacer regions of length L_{aS} and L_{aD} are used to isolate the gate silicide from the source/drain silicides. For the MESFET used as the output pass transistor of the linear regulator $L_g = L_{aS} = L_{aD} = 200\text{nm}$, $W_g = 152.2\text{nm}$ and the device had a soft breakdown voltage of $>5\text{V}$.

T. Thornton *et al.*, 2013 IEEE Radiation Effects Data Workshop (REDW), July 2013



Device data

- ◆ TID irradiation using cobalt-60, up to 1 Mrad(Si) (50, 100, 300, 500, 1000 krad)
- ◆ Slight degradation in efficiency, but very little change in either device
- ◆ Optocouplers sensitive to displacement damage – rad hard optocouplers under development





Next Steps

Present activities

- ◆ New program to develop next gen optocouplers
 - ◆ Lower R_{series}
 - ◆ Improved quantum efficiency
 - ◆ High radiation tolerance
- ◆ Develop advanced packaging – 2.5D and 3D schemes to reduce footprint, Hi-rel packages
- ◆ Able to provide prototypes for evaluation – or custom builds for particular specs

Acknowledgements

- ◆ Sponsors: NSF, AFWERX, DoD, VIPC CCF
- ◆ Collaborators:
 - ◆ Prof T. Grassman, A. Price, D. Hollingshead, L. Kaliszewski at OSU
 - ◆ Prof. R King, N. Irvin, Y. Lisova, C. Gregory, A. Chichalkar, E. Chen at ASU
 - ◆ Prof T. Thornton at ASU/RF Micropower
 - ◆ S. Buchner, radiation effects consultant



Thank you

mlumb@polarissemiconductor.com

(703) 225-9847